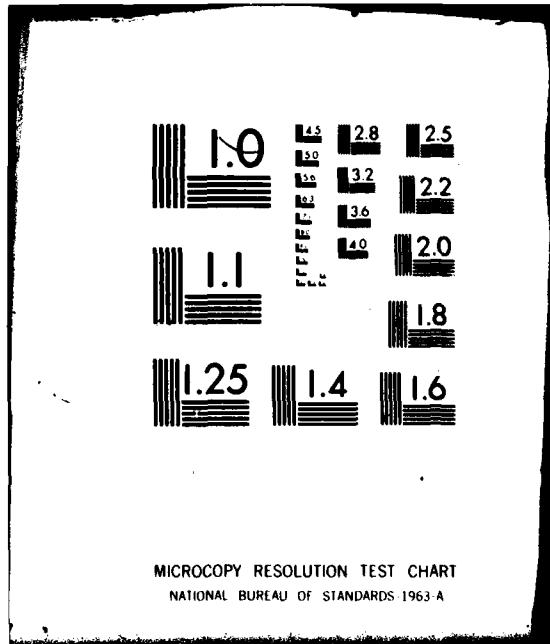


AD-A092 253

DOCKWELL INTERNATIONAL THOUSAND OAKS CA SCIENCE CENTER F/G 11/2
RESEARCH OF MICROSTRUCTURALLY DEVELOPED TOUGHENING MECHANISMS I--ETC(U)
ACT 80 F F LANGE N00014-77-C-0841
UNCLASSIFIED NL
CC5117.STR



END
DATE
FILED
1-8
DTIC



— SC5117.8TR —

102
SC5117.8TR

Copy No. 10

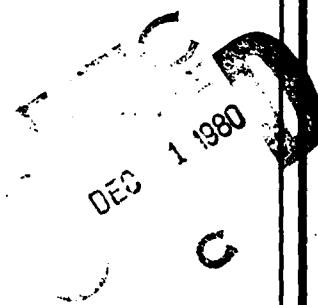
AD A092253

RESEARCH OF MICROSTRUCTURALLY DEVELOPED TOUGHENING MECHANISMS IN CERAMICS

TECHNICAL REPORT NO. 8

STRESS INDUCED TRANSFORMATION TOUGHENING, PART 1:
SIZE EFFECTS ASSOCIATED WITH CONSTRAINED
PHASE TRANSFORMATION THERMODYNAMICS

General Order No. 5117
Contract No. N00014-77-C-0441



F. F. Lange
Principal Investigator

October 1980

Approved for public release; distribution unlimited



Rockwell International
Science Center

DDC FILE COPY

80 11 28 003

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

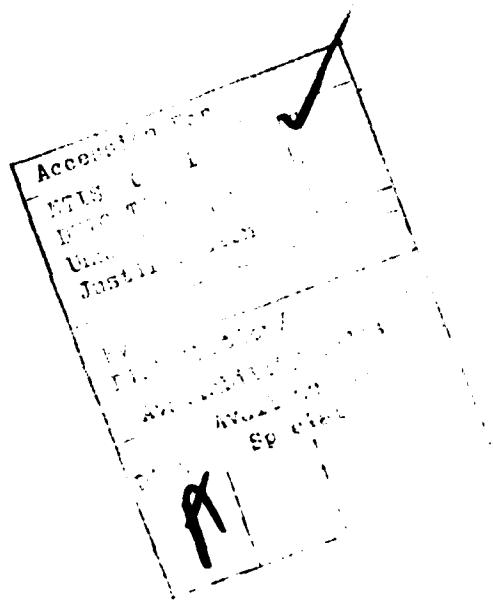
REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and subtitle) RESEARCH OF MICROSTRUCTURALLY DEVELOPED TOUGHENING MECHANISMS IN CERAMICS. Stress Induced Transformation Toughening, Part 1 Size Effects Associated with Constrained Phase Transformation Thermodynamics.		5. TYPE OF REPORT & PERIOD COVERED Technical Report No. 8
		6. PERFORMING ORG. REPORT NUMBER ASC5117.8TR
7. AUTHOR(s) F. F. Lange		7. CONTRACT OR GRANT NUMBER(s) N00014-77-C-0441
8. PERFORMING ORGANIZATION NAME AND ADDRESS Rockwell International Science Center 1049 Camino Dos Rios Thousand Oaks, CA 91360		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Project No. 032-574 (471)
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research 800 N. Quincy Street Arlington, VA 22217		12. REPORT DATE October 1980
13. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		14. NUMBER OF PAGES 27
15. SECURITY CLASS. (of this report) Unclassified		
16. DECLASSIFICATION/DOWNGRADING SCHEDULE		
17. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
18. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
19. SUPPLEMENTARY NOTES		
20. KEY WORDS (Continue on reverse side if necessary and identify by block number) Transformation Toughening ZrO₂ Phase Transformation Size Effect Strain Energy		
21. ABSTRACT (Continue on reverse side if necessary and identify by block number) The thermodynamics of the constrained phase transformation is presented with particular reference to size effects introduced by surface phenomena concurrent with the transformation, e.g., the formation of solid-solid surfaces (twins, etc.) and solid-vapor surfaces (e.g., microcracks). It is shown that these surface phenomena not only introduce a size-dependent energy term into the total free energy change, but also reduce the strain energy associated with the transformation, which can result		

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

20. ABSTRACT

in a transformation at a temperature where $|\Delta G^C|$ (the chemical free energy change) < ΔU_{rel} (the unrelieved strain energy associated with the constrained transformation). The results of this analysis lead to a phase diagram representation that includes the size of the transforming inclusion. This diagram can be used to define the critical inclusion size required to prevent the transformation and/or to obtain the transformation, but avoid one or more of the concurrent surface phenomena.



Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)



Rockwell International

Science Center

SC5117.8TR

STRESS INDUCED TRANSFORMATION TOUGHENING

PART I: SIZE EFFECTS ASSOCIATED WITH THE THERMODYNAMICS OF CONSTRAINED TRANSFORMATIONS

F.F. Lange

Structural Ceramics Group
Rockwell International Science Center
Thousand Oaks, California 91360

Abstract

The thermodynamics of the constrained phase transformation is presented with particular reference to size effects introduced by surface phenomena concurrent with the transformation, e.g., the formation of solid-solid surfaces (twins, etc.) and solid-vapor surfaces (e.g., microcracks). It is shown that these surface phenomena not only introduce a size dependent energy term into the total free energy change, but also reduce the strain energy associated with the transformation, which can result in a transformation at a temperature where $|\Delta G^c|$ (the chemical free energy change) < U_{se} (the unrelieved strain energy associated with the constrained transformation). The results of this analysis lead to a phase diagram representation that includes the size of the transforming inclusion. This diagram can be used to define the critical inclusion size required to prevent the transformation and/or to obtain the transformation, but avoid one or more of the concurrent surface phenomena.



Rockwell International
Science Center
SC5117.8TR

1.0 INTRODUCTION

It has been shown that a stress-induced, phase transformation can be used to increase the fracture toughness of brittle materials based on ZrO₂.⁽¹⁻⁵⁾ Metastable, tetragonal ZrO₂ is the toughening agent. Transformation to its stable, monoclinic structure in the vicinity of the crack front is believed to be responsible for the increased fracture toughness. In fabricating these tougher materials, it has been found that retention of the tetragonal structure to room temperature (or below) is critically dependent on the size of the microstructure. Namely, a critical gain size or inclusion size exists, below which the high temperature tetragonal phase can be retained and above which retention is not observed.

Two questions arise from these observations: 1) How can the tetragonal structure be retained upon cooling from its fabrication temperature when it usually undergoes a transformation? 2) How does the stress-induced transformation contribute to fracture toughness? In this part of a series of articles, the theoretical aspects of phase retention will be presented by examining the factors that affect the thermodynamics of a constrained phase transformation. Other articles in this series will address the theory of the toughening phenomena and experimental aspects concerned with phase retention and fracture toughness for materials in the ZrO₂-Y₂O₃ and Al₂O₃-ZrO₂ systems.



Rockwell International
Science Center
SC5117.8TR

2.0 THE $ZrO_2(t) + ZrO_2(m)$ TRANSFORMATION

Although the preceding sections are general for any transformation, the $ZrO_2(t) + ZrO_2(m)$ transformation will be used as an example. The tetragonal + monoclinic transformation in this system is athermal, diffusionless and involves both a shear strain and a volume change. The reader is referred to reviews by Subbarao et al⁶ and Heuer and Nord⁷ for details. Although some differences of opinion exists, Bailey,⁸ Bansal and Heuer,⁹ and more recently, Buljan et al¹⁰ have shown that the orientation relation between the monoclinic and tetragonal (fcc) unit cells is given by $(110_m) \parallel \{100_t\}$ and $[100_m] \parallel [001_t]$, which can be represented by the "stress-free" or unconstrained strain tensor

$$\tilde{\epsilon}^t = \begin{pmatrix} \frac{a_m \cos(\frac{90-\beta}{2}) - a_t}{a_t} & 0 & \tan(\frac{90-\beta}{2}) \\ 0 & \frac{b_m - a_t}{a_t} & 0 \\ \tan(\frac{90-\beta}{2}) & 0 & \frac{c_m \cos(\frac{90-\beta}{2}) - c_t}{c_t} \end{pmatrix} \quad (1)$$

where a , b , c are the cell dimensions of the respective tetragonal (t) and monoclinic (m) structures, and β ($<90^\circ$) is the monoclinic angle. Substituting the appropriate crystallographic data into Eq. (1), it can be shown that the transformation involves a large shear strain (~ 8%) and a substantial volume increase (3 - 5%).*

*The crystallographic data of Pratil and Subbarao⁽¹¹⁾ can be extrapolated to room temperature to show that the volume increase changes from 3% at 1150°C to 4.5% at room temperature; β is relatively insensitive to temperature.



Rockwell International
Science Center
SC5117.8TR

During cooling, the tetragonal \rightarrow monoclinic transformation of pure ZrO_2 begins at $\sim 1200^\circ C$ and proceeds over a temperature range (e.g., 1200° to $\sim 600^\circ C$) until the transformation is complete.⁶ Alloying oxides (e.g., Y_2O_3 , CeO_2 , etc.) lower the transformation temperature. In this regard, the $ZrO_2 - Y_2O_3$ system has been best studied. Srivastava et al¹² have shown that additions of Y_2O_3 to ZrO_2 lowers the transformation temperature to $565^\circ C$ where a eutectoid exists at ~ 3.0 m/o Y_2O_3 . Scott¹³ and Stubican et al¹⁴ appear to be in agreement.

3.0 THERMODYNAMICS OF A CONSTRAINED TRANSFORMATION

Classical theory has shown that retention of the tetragonal structure depends on the magnitude of the strain energy arising from the elastic constraint imposed by surrounding material on shape and volume changes associated with the transformation. Constraint can arise from several sources. First, if the polycrystalline body is single phase, neighboring grains, each with a different crystallographic orientation, will constrain the anisotropic strain of one another. Second, the transforming phase can similarly be constrained by a second phase matrix, as for the case of a two-phase material. The strain energy arising from these constraints can be reduced by microcracking and/or plastic deformation (e.g., twinning). Namely, both microcracking and twinning can accommodate some of the volume and shape change associated with the transformation and can reduce the constraint imposed by the surrounding material. Thus, as will be shown, retention of the tetragonal phase not only depends on the elastic properties of constraining material, but also on the possible occurrence of microcracking and/or twinning during transformation.



Rockwell International
Science Center

SC5117.8TR

3.1 Chemical Free Energy vs Strain Energy

To examine the thermodynamics of the constrained $ZrO_2(t)_2 + ZrO_2(m)$ reaction, let us first consider a stress-free, spherical inclusion of the tetragonal phase embedded within a matrix material as shown in Fig. 1a. On transforming to its monoclinic phase,* a state of stress arises within both the transformed inclusion and the surrounding matrix because of the constrained volume and shape change. The differential free energy (ΔG_{t+m}) between these two states per unit volume of transformed material is

$$\Delta G_{t+m} = G_m^C - G_t^C + U_{se}^m - U_{se}^t + U_s^m - U_s^t$$

or

$$\Delta G_{t+m} = -\Delta G^C + \Delta U_{se} + \Delta U_s \quad . \quad (2)$$

where ΔG^C is the chemical free energy (dependent on temperature and composition), ΔU_{se} is the strain energy associated with the transformed particle (for the case considered here $U_{se}^t = 0$ and $\Delta U_{se} = U_{se}^m$) and surrounding matrix which is usually less sensitive to temperature and composition, and ΔU_s is the change in energy associated with the inclusion's surface.

*It is assumed throughout this paper that the whole inclusion transforms in a spontaneous and uniform manner. Although this assumption neglects the conditions for the nucleation and growth usually associated with these transformations, it does allow us to examine the limiting condition concerning the thermodynamic stability of the constrained inclusion.



Rockwell International
Science Center
SC5117.8TR

SC80-9951

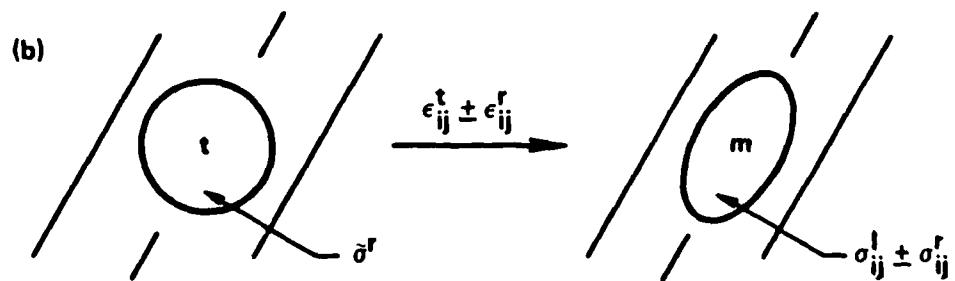
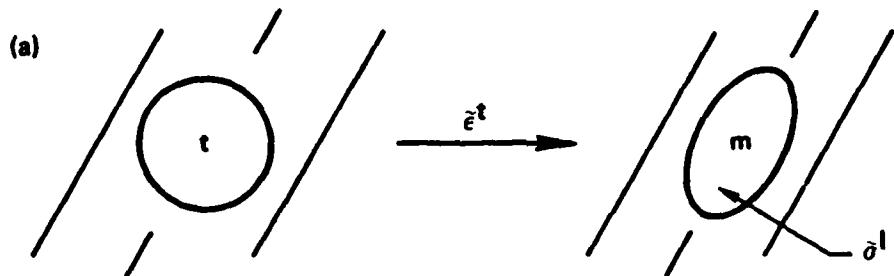


Fig. 1 a) Constrained transformation where initial state (*t*) is stress free,
b) initial state under residual stress (σ_r).



Rockwell International
Science Center
SC5117.8TR

The condition for the transformation requires that $\Delta G_{t+m} < 0$, or from Eq. (2)*

$$|\Delta G^c| > U_{se}^m + \Delta U_S \quad . \quad (3)$$

It can be seen that since U_{se}^m is always positive, the constrained transformation temperature will be lower than for the unconstrained case ($|\Delta G^c| > U_S$). That is, constraint lowers the transformation temperature.

The magnitude of the strain energy will depend on the elastic properties of the transformed inclusion and the surrounding matrix, the inclusion shape, and the transformation strain. Eshelby⁽¹⁵⁾ has shown that

$$U_{se}^m = \frac{1}{2} \sigma_{ij}^I \epsilon_{ij}^t \quad (4)$$

where $\tilde{\sigma}^I$ defines the uniform stress state within the transformed inclusion, and $\tilde{\epsilon}^t$ is the "stress-free" transformation strain (e.g., given by Eq. (1) for $ZrO_2(t) \rightarrow ZrO_2(m)$).

The effect of the elastic properties of the constraining matrix can be examined by assuming that the transformation only involves an isotropic volume expansion, viz $\epsilon_{ij}^t = \frac{1}{3} \Delta V/V \delta_{ij}$. With this assumption it can be shown that for the case of a sphere

*Throughout this paper, only temperatures where ΔG^c is negative are considered, thus $-\Delta G^c$ is written as $|\Delta G^c|$ for convenience.



Rockwell International
Science Center
SC5117.8TR

$$U_{se}^m = \frac{k}{6} \left(\frac{\Delta V}{V} \right)^2 , \quad (5)$$

where

$$k = \frac{2E_1 E_2}{(1 + v_1)E_2 + 2(1 - 2v_2)E_1} \quad (6)$$

and $E_{1,2}$, $v_{1,2}$ are Young's modulus and Poisson's ratio of the matrix (1) and transforming particle (2). That is, the greater the elastic modulus of the constraining matrix, the greater the strain energy and, thus, the lower the potential transformation temperature, i.e., the constrained transformation temperature will be inversely proportional to the rigidity of the constraining matrix.*

Alloy additions that lower the unconstrained transformation temperature (i.e., additions such as Y_2O_3 that decrease $|\Delta G^c|$) will also lower the constrained transformation temperature.

3.2 Effect of Residual Stresses

In the preceding section it was assumed that the initial tetragonal state was free of residual stresses. This is not the normal situation since residual stresses will arise during fabrication (e.g., during cooling from the

*It should be pointed out here that the strain energy term in Eq. (2) is only significant for reactions involving relatively small changes in chemical free energy (< several Kcal/mol). It is usually neglected for most chemical reactions where $|\Delta G^c| \gg \Delta U_{se}$.



Rockwell International
Science Center
SC5117.8TR

fabrication temperature as a result of thermal expansion mismatch with the matrix phase). As will be shown, these residual stresses will either increase or decrease the strain energy term in Eq. (2) and thus influence the potential transformation temperature.

Figure 1b illustrates the spherical tetragonal inclusion in a state of residual stress and its transformed, monoclinic state. The residual stress state is defined by $\tilde{\sigma}^r$ which, according to Eshelby, arises from a "stress-free" strain $\tilde{\epsilon}^r$, e.g., the strain an unconstrained inclusion would exhibit due to thermal contraction. The strain energy associated with the tetragonal state is

$$U_{se}^t = \frac{1}{2} \sigma_{ij}^r \epsilon_{ij}^r . \quad (7)$$

Using the principle of superposition, it can be shown that the strain energy in the transformed, monoclinic state is

$$U_{se}^m = \frac{1}{2} (\sigma_{ij}^I + \sigma_{ij}^r)(\epsilon_{ij}^t + \epsilon_{ij}^r) , \quad (8)$$

where $\tilde{\sigma}^I$ and $\tilde{\epsilon}^t$ are those stresses and strains defined earlier for the transformation from an unstressed tetragonal particle. The \pm sign in front of the residual stress/strain terms in Eq. (8) is to remind the reader that the individual components of these tensors can have either the same sense (+) or the opposite sense (-) relative to the components associated with the transformation.

The free energy change associated with the transformation shown in Fig. 1b is



Rockwell International

Science Center

SC5117.8TR

$$\Delta G_{t \rightarrow m} = -\Delta G^C + U_{se}^m - U_{se}^t + \Delta U_S \quad . \quad (9)$$

Substituting Eqs. (7) and (8) into (9):

$$\Delta G_{t \rightarrow m} = -\Delta G^C + U_{se}^0 \pm \sigma_{ij}^I \epsilon_{ij}^r \pm \sigma_{ij}^r \epsilon_{ij}^t + \Delta U_S \quad , \quad (10)$$

where U_{se}^0 is the strain energy defined by Eq. (4) for the case where the tetragonal particle is initially stress free.

Equation (10) illustrates that the residual stress and strain fields either increase or decrease the strain energy depending on their sense. That is, if the transformational fields are compressive and the initial residual fields are tensile, the strain energy is diminished. If, on the other hand, the residual field has the same sense as the transformational field, the strain energy is increased. This latter case will decrease the transformation temperature.

4.0 EFFECT OF INCLUSION SIZE

As mentioned in the Introduction, experiments have shown that the retention of tetragonal ZrO_2 is size dependent. That is, a critical inclusion/grain size exists, below which retention can be achieved and above which it cannot. This size effect cannot be explained by the approach discussed above. What is required is a term in the free energy expression (viz Eq. 2) which includes the size of the transforming volume.



4.1 Influence of ΔU_s

The change in the surface energy per unit volume (V) of a transformed spherical inclusion can be expressed as

$$\Delta U_s = \Delta A(\gamma_m - \gamma_t) / V = 6\left(\frac{\Delta A}{A}\right)(\gamma_m - \gamma_t) / D , \quad (11)$$

where ΔA is the change in the particle's surface area, γ_m and γ_t are the specific interfacial surface energies in the transformed and untransformed states, and A and D are the area and diameter of the transformed particle, respectively. Substituting Eq. (7) into Eq. (3) and rearranging, it can be seen that the surface energy term introduces a size effect, i.e., a critical particle size (D_c) above which the energetics of the transformation are stabilized (viz $\Delta G_{t-m} < 0$) and the transformation can proceed,

$$D > D_c = \frac{6\left(\frac{\Delta A}{A}\right)(\gamma_m - \gamma_t)}{[|\Delta G^c| - \Delta U_{se}]} . \quad (12)$$

Garvie⁽¹⁶⁾ has used a similar argument to explain the experimental observation that unconstrained tetragonal ZrO₂ powders are obtained at room temperature when produced with a particle size < 300 Å. In order to explain this size effect with the surface energy term, Garvie had to assume that $\gamma_m > \gamma_t$.^{*} Based on this assumption and the condition that $\Delta U_{se} = 0$ for the case of

*Garvie neglected the possibility of internal surface (twins) in the transformed particles which would have produced the same effect without the assumption that $\gamma_m > \gamma_t$.



Rockwell International
Science Center
SC5117.8TR

unconstrained powders, the critical particle size (D_{uc}) for the powder is

$$D_{uc} = \frac{6(\frac{\Delta A}{A})(\gamma_m - \gamma_t)}{|\Delta G^c|} . \quad (13)$$

Substituting Eq. (13) into (12) and rearranging, the critical size for the constrained state can be related to the critical size for the unconstrained state by

$$D_c = \frac{D_{uc}}{1 - \frac{\Delta U_{se}}{|\Delta G^c|}} . \quad (14)$$

Examination of Eq. (14) shows that a critical size does exist when $|\Delta G^c| > \Delta U_{se}$ and that $D_c > D_{uc}$.

4.2 Loss of Constraint Through Microcracking and Twinning

As mentioned above, both microcracking and twinning can accompany the $ZrO_2(t) \rightarrow ZrO_2(m)$ transformation. Microcracking and twinning both relieve some of the constraint associated with the volume change and shape change, respectively. In both cases, relief of constraint decreases the strain energy associated with the transformation. As will be shown, the occurrence of microcracking and/or twinning results in a size effect for cases when $|\Delta G^c| < \Delta U_{se}$.

Let us first consider the case of microcracking. Assume that during transformation, a small flaw at the inclusion/matrix interface extends and becomes an arrested microcrack, as shown in Fig. 2a (see Refs. 17, 18 and 19 for the growth requirements of such a crack). A radial crack would be a likely type



Rockwell International
Science Center
SC5117.8TR

SC80-9952

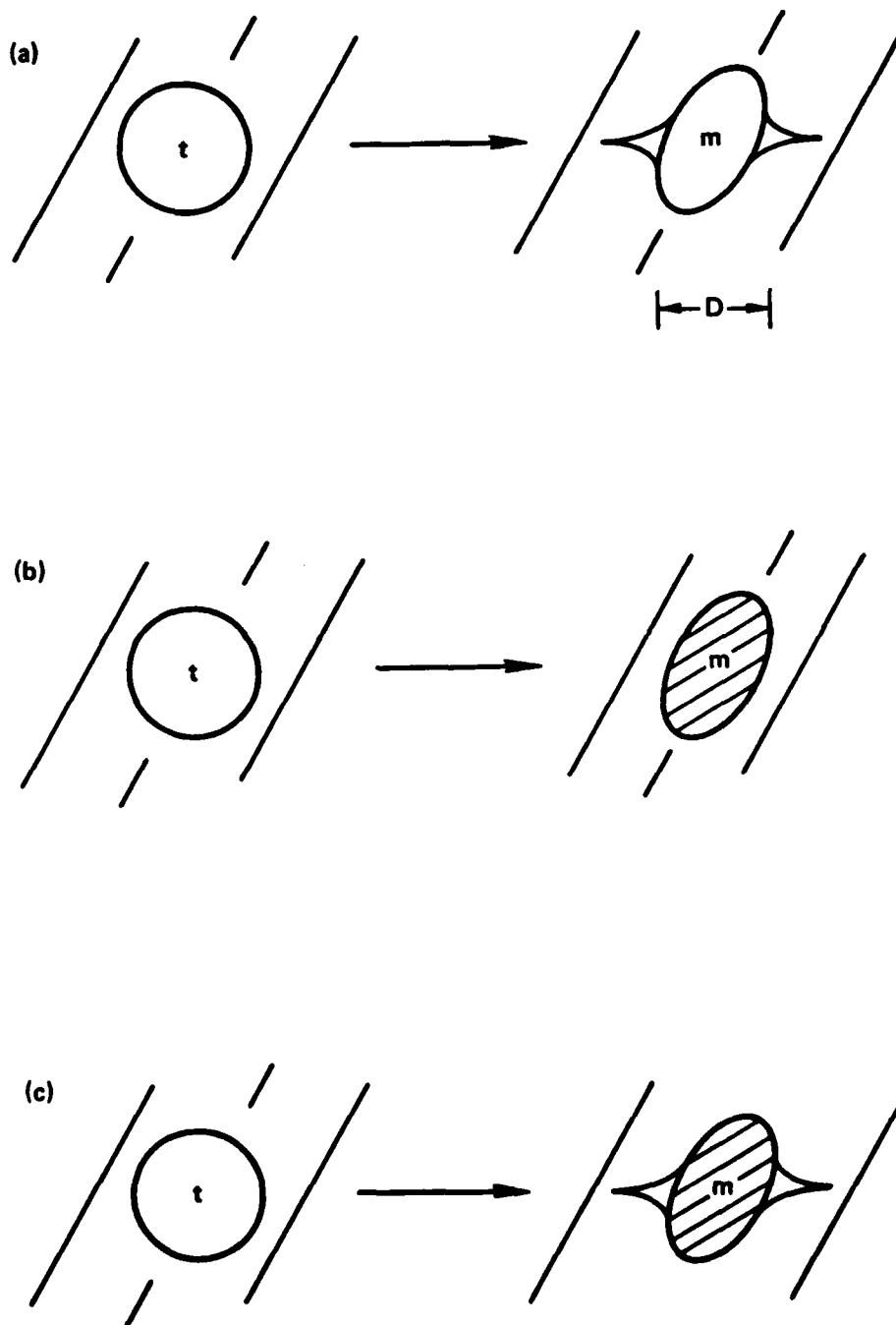


Fig. 2 a) Transformation + microcracking, b) transformation + twinning,
c) transformation + microcracking + twinning.



Rockwell International

Science Center

SC5117.8TR

of crack due to the volume expansion associated with the transformed ZrO_2 inclusion. The presence of the crack will change the energetics of the transformed particle in two respects. First, the crack will relieve a fraction $(1 - f_c)$ of the strain energy, ΔU_{se} , associated with the uncracked, transformed system. Second, the crack introduces new surface.

The change in free energy of this microcracked system can be written as follows:

$$\Delta G_{t+m} = -\Delta G^c + \Delta U_{se} f_c + \frac{A_c \gamma_c}{V} + \Delta U_s . \quad (15)$$

The second from last term in Eq. (15) is the energy per unit volume of transformed material associated with the crack surface; A_c is the area of the crack surfaces, γ_c is the fracture energy per unit area, and V is the volume of the particle. By defining the area of the arrested crack with respect to the inclusion's surface ($A_c = \pi D^2 g_c$) and using $V = 6\pi D^3$, Eq. (15) can be rewritten as

$$\Delta G_{t+m} = -\Delta G^c + \Delta U_{se} f_c + \frac{6\gamma_c}{D} g_c + \frac{6(\frac{\Delta A}{A})(\gamma_m - \gamma_t)}{D} . \quad (16)$$

Both f_c and g_c are numerical values that depend on the size of the arrested crack. Previous work^(18,19) has shown that f_c and g_c are weak functions of the initial flaw size responsible for the extended microcrack.

Equation (16) shows that the size of the transformed particle is now contained in two terms, i.e., one associated with the energy due to the crack and the other associated with the energy due to the inclusion's surface. Again,



Rockwell International
Science Center
SC5117.8TR

the transformation will only proceed when $\Delta G_{t+m} < 0$, which from rearranging Eq. (16) defines a critical size for transformation and microcracking.

$$D > D_c^C = \frac{6[\gamma_c g_c + \frac{\Delta A}{A}(\gamma_m - \gamma_t)]}{|\Delta G^C| - \Delta U_{se} f_c} \quad (17)$$

Examination of Eq. (17) shows that the size effect for transformation and microcracking exists when $|\Delta G^C| > \Delta U_{se} f_c$.

Let us now consider the conditions for transformation and twinning (Fig. 2b). In a manner similar to that discussed for microcracking, the energetics of the constrained transformation in which the transformed particle twins can be written as

$$\Delta G_{t+m} = -\Delta G^C + \Delta U_{se} f_t + \frac{6\gamma_t g_t}{D} + \Delta U_s \quad (18)$$

The second from the last term is the energy of the twin surface per unit volume of transformed material. Here, the total area of the twin boundaries (A_t) is normalized by the particle's surface area ($g_t = A_t/\pi D^2$). The factors f_t and g_t are dimensionless values, $f_t < 1$, $g_t > 0$; γ_t is the twin boundary energy per unit area.

Similar in all respects to the microcracking phenomena, a critical particle size exists, above which transformation and twinning is possible:

$$D > D_c^t = \frac{6\gamma_t g_t + \frac{\Delta A}{A}(\gamma_m - \gamma_t)}{|\Delta G^C| - \Delta U_{se} f_t} \quad (19)$$

Again, this size effect only exists for the condition $|\Delta G^C| > \Delta U_{se} f_t$.



Rockwell International
Science Center
SC5117.8TR

Now let us consider the case where both microcracking and twinning accompanies the transformation, as shown in Fig. 2c. By using the same approach, it can be shown that a critical inclusion size exists, above which transformation, microcracking and twinning is possible:

$$D > D_{c,t}^c = \frac{6 \gamma_c g_c + \gamma_t g_t + \frac{\Delta A}{A} (\gamma_m - \gamma_t)}{|\Delta G^c| - \Delta U_{se}^{fcft}} . \quad (20)$$

Likewise, the condition where this size effect will be observed is $|\Delta G^c| > \Delta U_{se}^{fcft}$.

5.0 DISCUSSION

Classical theory of constrained phase transformations, as outlined in the first part of this paper, shows that the potential for lowering the transformation temperature primarily resides with the magnitude of the strain energy that would arise if the transformation were to proceed. For a given transformation, the strain energy depends on the elastic properties of the constraining matrix and the residual strains that pre-exist in the untransformed state. The strain energy can be maximized by maximizing both the elastic properties of the constraining matrix and the pre-existing residual strains which must have the same sense as the transformational strains. Residual strains of opposite sense decrease the strain energy. For the case of ZrO₂, the ideal constraining matrix would not only have a high elastic modulus, but a higher thermal expansion coefficient than tetragonal ZrO₂.



Rockwell International
Science Center
SC5117.8TR

The constrained transformation temperature can also be decreased by decreasing the change in chemical free energy ($|\Delta G^c|$). This can be accomplished by alloying with an additive (e.g., Y_2O_3 , CeO_2 , etc.) that is known to decrease the unconstrained transformation temperature.

In addition to these more classical results, it has been shown that the thermodynamics of the constrained transformation depend on the size of the transforming volume. This size effect is introduced through surface changes associated with the transformation. Three different surface related phenomena, viz. microcracking, twinning and microcracking combined with twinning, have the potential for producing a size effect for conditions where $|\Delta G^c| < \Delta U_{se}$. An additional size effect can arise when $|\Delta G^c| > \Delta U_{se}$ due to the changes associated with the inclusion/matrix interfacial energy. The question is now -- which of these size effects is most critical and best explains the experimental observations.

Equations (17), (19), and (20) can be rearranged to express the normalized critical particle sizes for

a) microcracking

$$\frac{D_c}{D_{uc}} = \frac{\frac{1 + \frac{\gamma_c g_c}{\Delta A (\gamma_m - \gamma_t)}}{1 - \frac{\Delta U_{se} f_c}{|\Delta G^c|}}}{.} \quad (21)$$

b) twinning

$$\frac{D_c}{D_{uc}} = \frac{\frac{1 + \frac{\gamma_t g_t}{\Delta A (\gamma_m - \gamma_t)}}{1 - \frac{\Delta U_{se} f_t}{|\Delta G^c|}}}{. \text{ and}} \quad (22)$$



Rockwell International
Science Center

SC5117.8TR

c) microcracking plus twinning

$$\frac{D_{c,t}}{D_{uc}} = \frac{1 + \frac{\gamma_c g_c + \gamma_t g_t}{\frac{\Delta A}{A} (\gamma_m - \gamma_t)}}{1 - \frac{\Delta U_{se} f_c f_t}{|\Delta G^c|}} \quad (23)$$

where D_{uc} is the critical particle size for unconstrained powders as defined by Eq. (13). By making reasonable assumptions concerning the values of f_c , f_t and relative values for the surface energy terms, one can obtain a comparison between Eq. (14), (21), (22) and (23) to judge the dominant size effects.

Recent results of Ito et al.,⁽¹⁹⁾ have shown that a single radial crack in its arrest position relieves ~ 10% of the strain energy associated with the residual stress field of a spherical inclusion. Thus, a value of $f_c = 0.9$ was chosen. Porter⁽²⁰⁾ has calculated that ~ 70% of the strain energy for the constrained ZrO_2 transformation is associated with the shear strain. Twinning is expected to relieve a large portion, and thus a value of $f_t = 0.67$ was chosen, i.e., it was assumed that 33% can be relieved by twinning. Concerning the surface energy terms, it is reasonable to assume that the cracks' surface energy is greater than both the twin surface energy and the differential interfacial energy of the two states, i.e., $\gamma_c g_c > \gamma_t g_t = \frac{\Delta A}{A} (\gamma_m - \gamma_t)$. Values chosen are:

$$\frac{\gamma_c g_c}{\frac{\Delta A}{A} (\gamma_m - \gamma_t)} = 10$$

and

$$\frac{\gamma_t g_t}{\frac{\Delta A}{A} (\gamma_m - \gamma_t)} = 1$$



Rockwell International

Science Center

SC5117.8TR

Substituting the values of these parameters into Eqs. (14), (21), (22) and (23), the normalized particle size was plotted as a function of $\Delta U_{se}/\Delta G^c$, as shown in Fig. 3.

Figure 3 maps the size requirements for retaining the tetragonal phase and indicates the type of strain energy relieving phenomena (e.g., twinning, microcracking) that would be observed if these requirements are not met. Since ΔU_{se} is much less dependent on temperature and alloying composition relative to ΔG^c , the axis of abscissas in Fig. 3 can either represent increasing temperature or increasing alloy composition.

It should first be noted that the normalized critical size for each phenomena $\rightarrow \infty$ at the temperature where $|\Delta G^c| = \Delta U_{se}$ the relieved strain energy. Also, the rate in which the critical size decreases with temperature is controlled by the numerator of each function. For a given ZrO₂ alloy, the first size effect encountered during cooling (decreasing $\Delta U_{se}/\Delta G^c$) will be that due to both microcracking and twinning which, when combined, results in the largest decrease in strain energy. At a given temperature where $|\Delta G^c| > \Delta U_{se} f_{ct}$, transformation will be accompanied by both microcracking and twinning when the normalized size of the transforming inclusion lies above the curve labeled microcracking + twinning. With a further decrease in temperature, i.e., when $|\Delta G^c| > U_{se} f_t$, the size effect for transformation and twinning arises. Normalized particle sizes that fall within the area bounded by the twinning only and microcracking + twinning curves will be transformed and twinned. Figure 3 shows that the condition for transformation and microcracking (at temperatures where $\Delta G^c > \Delta U_{se} f_c$) is only of academic interest. This size requirement is less stringent than the previous two. The last size effect, i.e., due



Rockwell International

Science Center

SC5117.8TR

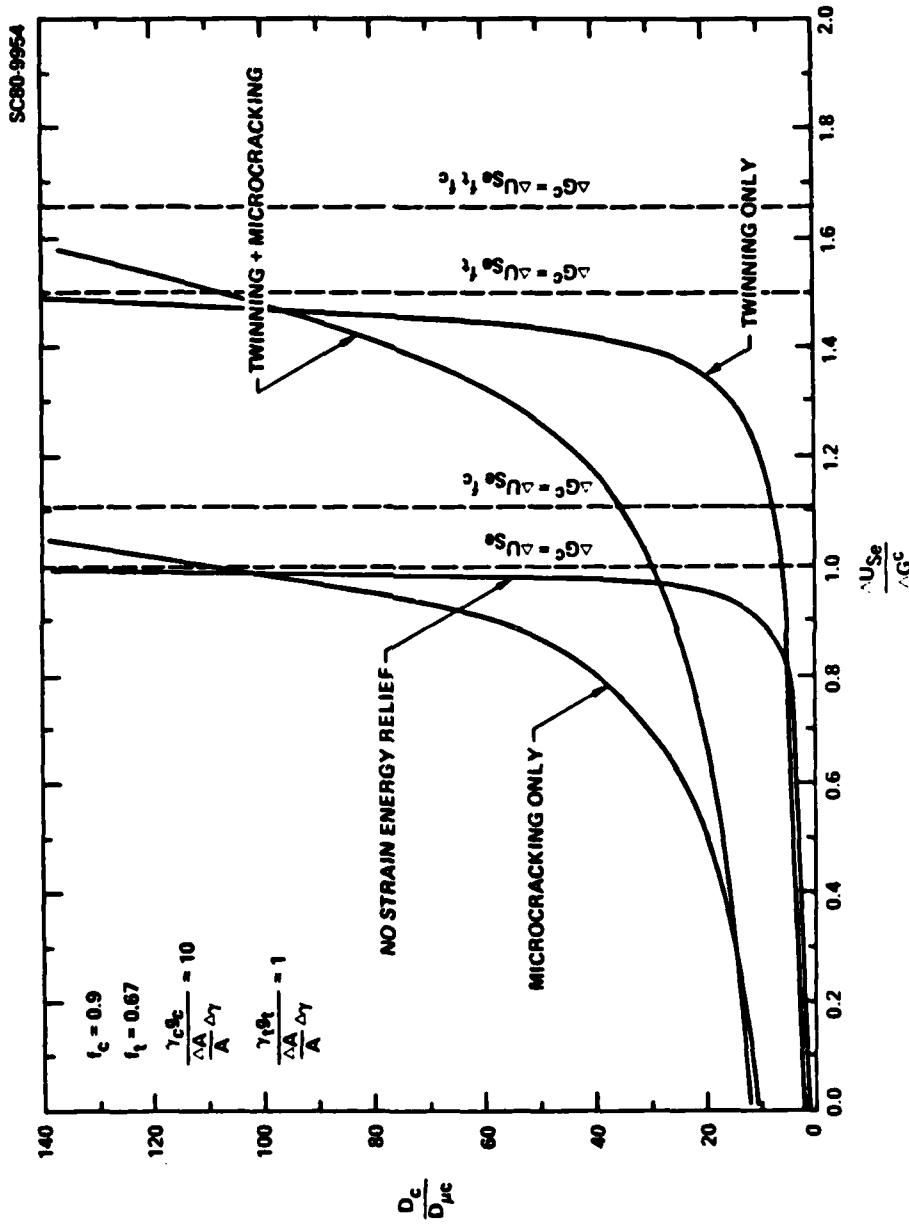


Fig. 3 Plot of conditions where $\Delta G_t = 0$ which includes various surface energy terms as represented in a normalized inclusion (grain) size vs strain energy (U_{Se})/chemical free energy (ΔG^c) space.



Rockwell International
Science Center
SC5117.8TR

to the change in interfacial energy, which can only occur at temperatures where $|\Delta G^C| > \Delta U_{se}$, has a limited phase field in Fig. 3 between the curves marked "Twinning Only" (upper bound) and "No Strain Energy Relief" (lower bound). This phase field indicates a limited inclusion size range for transformation without twinning and microcracking. (It should be noted that if $\gamma_t > \gamma_m$, the "No Strain Energy Relief" curve would be mirrored about the $\Delta U_{se}/\Delta G^C = 1$ line relative to that shown in Fig. 3 to form the lower bound of the tetragonal phase field.)

Since each of the functions illustrated in Fig. 3 defines conditions where $\Delta G_{t+m} = 0$, it is obvious that these functions define phase boundaries. Therefore, they can be used to construct a phase diagram to indicate the surface phenomena that will or will not accompany a transformation in normalized inclusion size - $\Delta U_{se}/\Delta G^C$ (e.g., temperature) space. As shown in Fig. 4, four phase fields are evident for the parameters used: 1) a tetragonal field, 2) a monoclinic + twinned + microcracked field, 3) a monoclinic + twinned field, and 4) a monoclinic field without twinning or microcracking. Unlike conventional phase diagrams, Fig. 4 includes the size of the inclusion that is introduced through the various surface energy terms. Although Fig. 4 is derived for specific parameters and would quantitatively change for other parameters, its general character (i.e., phase fields) will remain unchanged if $f_t > f_c$ and $\gamma_c g_c > \gamma_t g_t$.

The phase relations in Fig. 4 predict the following observations. On cooling a composite with a wide distribution of inclusion sizes to a temperature where $\Delta U_{se}/\Delta G^C = 1.2$, there will be a range of inclusions below a critical size still in their tetragonal state. Somewhat larger inclusions will be transformed



Rockwell International
Science Center
SC5117.8TR

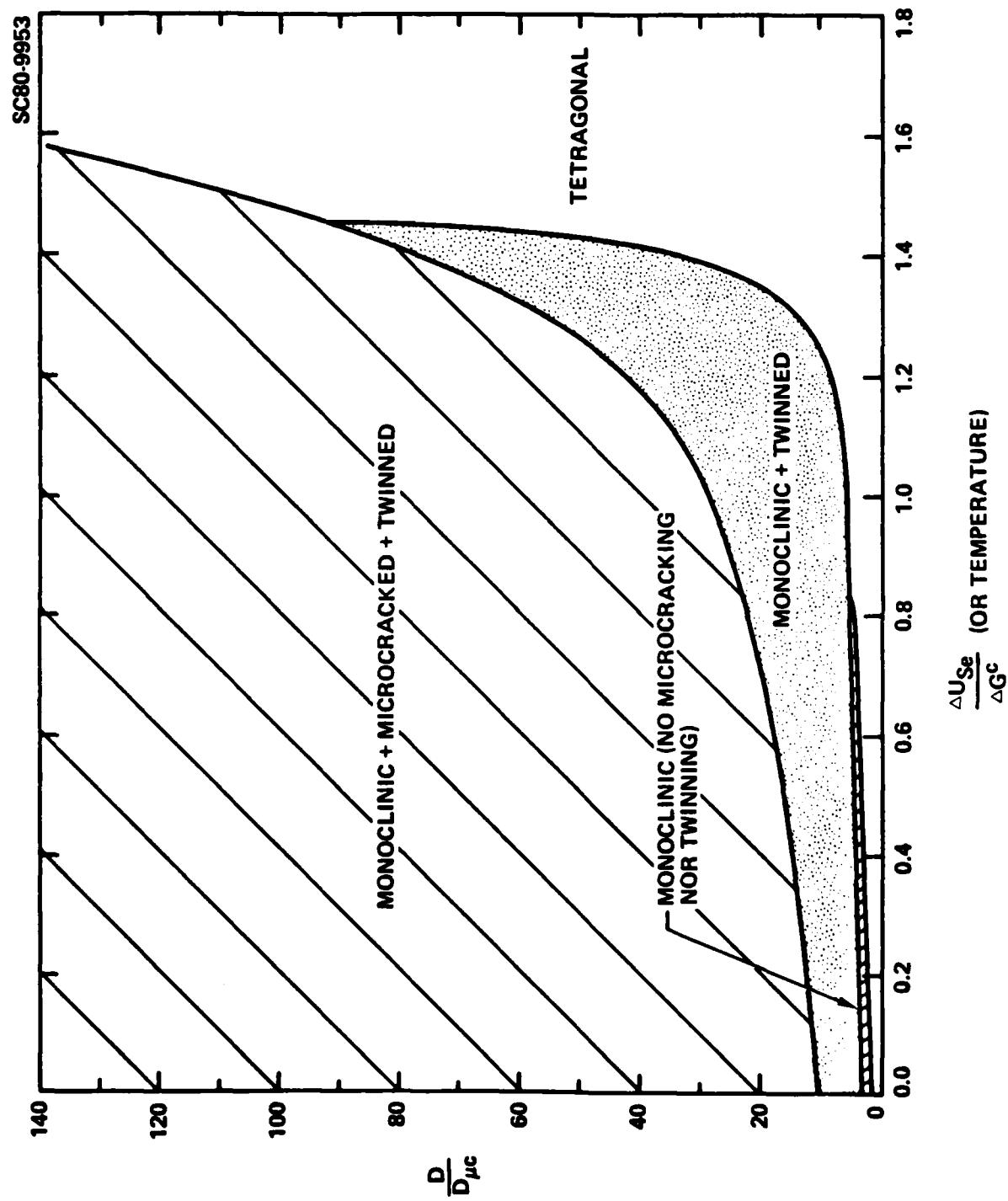


Fig. 4 Phase regions defined by Fig. 3 indicating conditions of transformation and associated surface phenomena as a function of normalized particle size vs temperature of alloy composition.



Rockwell International
Science Center

SC5117.8TR

and twinned, and still larger inclusions will be transformed, twinned and microcracked. If the same composite were only cooled to the temperature where $\Delta U_{sc}/\Delta G^c = 1.55$, inclusions larger than D_c would be transformed, twinned and microcracked; smaller inclusions will be untransformed. Composites with a very narrow size distribution would be in only one of these phase fields. If appropriate experimental techniques were developed to independently observe twinning and microcracking, a composite with a wide inclusion size distribution could be used to experimentally determine the phase boundaries in Fig. 4.

Since the abscissa can also represent increasing alloy composition at a fixed temperature, Fig. 4 can be used to determine the effect of changing alloy composition. For example, at a particular temperature and normalized inclusion size, an increase in alloy content would shift the transformation conditions from one phase field to another; an inclusion-size/composition phase diagram could be constructed at, e.g., room temperature, by heat treating a number of different alloy compositions to increase the inclusion size, and then observing the size required for transformation, twinning and microcracking.

Without specific knowledge of the phase boundaries, it is obvious that the size effects discussed above are critical in fabricating a material in which the object is to retain the high temperature phase upon cooling. If powder routes are used (i.e., sintering), powder sizes $< D_c$ are required since grain growth during sintering is inevitable. If a solid-solution precipitation route is used, heat treatment must be controlled to avoid precipitate growth $> D_c$. Thus, strict microstructural control is required to retain the high temperature phase below its unconstrained transformation temperature.



Rockwell International
Science Center

SC5117.8TR

On the other hand, the objective of fabrication may be to achieve the transformation but to avoid microcracking and/or twinning, as for the case of ferroelectrics. Ferroelectric materials are produced by constrained transformation. Twins (domains) form during the transformation, to primarily relieve strain energy (in non-conducting media, domains also reduce the external electric field due to polarization). Microcracking has also been observed to occur during transformations. The ferroelectric literature sites several grain size phenomena consistent with the agreements leading to Fig. 4. Matsuo and Sasaki⁽²¹⁾ showed that when $PbTiO_3$ is fabricated with a grain size $\sim 10 \mu m$, a highly microcracked body is produced upon cooling through its transformation temperature; a non-microcracked transformed material could be produced with a grain size of $< 3 \mu m$. Buessem et al,⁽²²⁾ indicate that as the grain size of $BaTiO_3$ is reduced to $\sim 1 \mu m$, twinning is prevented during the transformation which leads to a high permittivity. Thus, it can be seen that further work in defining phase fields shown in Fig. 4 are of importance for a variety of useful constrained phase transformations.

ACKNOWLEDGEMENTS

This work was supported by the Office of Naval Research under Contract N00014-77-C-0441. The author deeply appreciated discussions with his colleagues D.J. Green and D.R. Clarke.



Rockwell International

Science Center

SC5117.8TR

REFERENCES

1. R.C. Garvie, R.H. Hannick and R.T. Pascoe, Nature 258, 703 (1975).
2. R.C. Garvie and R.T. Pascoe, Processing of Crystalline Ceramics, ed. by H. Palmour III, R.F. Davis and T.M. Hare, p. 263, Plenum Press (1978).
3. D.L. Porter and A.H. Heuer, J. Am. Ceram. Soc. 60, 183 (1977); ibid. 280 (1977).
4. T.K. Gupta, J.H. Bechtold, R.C. Kuznichi, L.H. adoff and B.R. Rossing, J. Mat. Sci. 12, 2421 (1977).
5. T.K. Gupta, F.F. Lange and J.H. Bechtold, J. Mat. Sci. 13, 1464 (1978).
6. E.C. Subbarao, H.S. Maiti and K.K. Srivastava, Phys. Stat. Sol. 21, 9 (1974).
7. A. Heuer and G.L. Nord, Jr., Electron Microscopy in Mineralogy, ed. by H.R. Weuk, p. 274, Springer-Verlag (1976).
8. J.E. Bailey, Proc. Roy. Soc. 279A, 395 (1964).
9. G.K. Bansal and A.H. Heuer, Acta Met. 22, 409 (1974).
10. S.T. Buljan, H.A. McKinstry and V.S. Stubican, J. Am. Ceram. Soc. 59, 351 (1976).
11. R.N. Patil and E.C. Subbarao, J. Appl. Cryst. 2, 281 (1969).
12. K.K. Srivastava, R.N. Patil, C.B. Chaudary, K.V.G.K. Gokhale and E.C. Subbarao, Trans. Brit. Ceram. Soc. 73, 85 (1974).
13. H.G. Scott, J. Mat. Sci. 10, 1527 (1975).
14. V.S. Stubican, R.C. Hink and S.P. Ray, J. Am. Ceram. Soc. 61, 17 (1978).
15. J.D. Eshelby, Progress in Solid Mechanics, Vol. 2, ed. by I.N. Sneddon and R. Hill, p. 89, North-Holland (1961).
16. R.C. Garvie, J. Phys. Chem. 69, 1238 (1965); J. Phys. Chem. 82, 218 (1978).
17. F.F. Lange, Fracture Mechanics of Ceramics, ed. by R.C. Bradt, D.P.H. Hasselman, and F.F. Lange, Vol. 2, p. 599, Plenum Press (1974), ibid Vol. 4 p. 799 (1978).
18. Y.M. Ito, M. Rosenblatt, L.Y. Cheng, F.F. Lange and A.G. Evans, Inter. J. Fracture (in press).



Rockwell International
Science Center
SC5117.8TR

19. Y.M. Ito and F.F. Lange (to be published).
20. D.L. Porter, Ph.D. Thesis, Case-Western University (1977); University Microfilms Int. Order No. 77-25185, 190 pp.
21. Y. Matsuo and H. Sasaki, J. Am. Ceram. Soc. 49, 229 (1966).
22. W.R. Buessem, L.E. Cross and A.K. Goswanii, J. Am. Ceram. Soc. 49, 33 (1966).